

Reactor Physics Experiment NEA Benchmark Possibilities for Measurements at ORCEF and Other DOE Facilities



John T. Mihalcz

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Isotope and Fuel Cycle Technology Division

**REACTOR PHYSICS EXPERIMENT NEA BENCHMARK POSSIBILITIES FOR
MEASUREMENTS AT ORCEF AND OTHER DOE FACILITIES**

John T. Mihalczo

December 2019

Prepared by
OAK RIDGE NATIONAL LABORATORY
Oak Ridge, TN 37831-6283
managed by
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ACRONYMS

DOE	Department of Energy
LANL	Los Alamos National Laboratory
NEA	Nuclear Energy Agency
ORNL	Oak Ridge National Laboratory
ORCEF	Oak Ridge National Laboratory Critical Experiments Facility
PNNL	Pacific Northwest National Laboratory
Y-12 NSC	Y-12 National Security Complex

ABSTRACT

This report documents a wide variety of critical and subcritical reactor physics measurements that could be included in the Nuclear Energy Agency (NEA) *International Handbook of Evaluated Reactor Physics Benchmark Experiments*. The experiments were performed by John T. Mihalczko and coworkers at many (8) Department of Energy (DOE) facilities, including the Oak Ridge National Laboratory Critical Experiments Facility (ORCEF between 1958 and 1975); Los Alamos National Laboratory (LANL); Pacific Northwest National Laboratory; Babcock and Wilcox at Lynchburg, Virginia; and the Y-12 National Security Complex (Y-12 NSC) (the latter between 1975 and up to 2006). This report lists the various measurement programs and a limited description of the reactor physics measurements that were performed in each, which could serve as benchmarks. Some criticality safety measurements at these facilities have already been documented in the NEA *International Handbook of Evaluated Criticality Safety Benchmark Experiments*. Some of these reactor physics measurements have also been documented in the literature, and this document give a complete list of references for which John T. Mihalczko was an author or co-author. The experiments are divided into four classes: critical experiments only, critical and subsequent subcritical experiments, subcritical experiments at critical facilities, and subcritical measurements performed in material balance areas of the Y-12 NSC and other facilities. Because of the high cost and large amount of facility time related to these measurements, it is very cost-effective to mine the existing data to produce NEA reactor physics benchmarks. The information for many of these measurements is documented in critical experiment and subcritical experiment logbooks at the International Criticality Safety Benchmark Program at Idaho National Laboratory and in laboratory records at Oak Ridge National laboratory.

1. INTRODUCTION

Between 1958 and 2006, a wide variety of critical experiments and subcritical experiments were performed at eight different US DOE facilities, many at ORCEF. Many of the measurements were performed in critical experiment facilities. This report documents a wide variety of critical and subcritical reactor physics measurements that could be included in the NEA *International Handbook of Evaluated Reactor Physics Benchmark Experiments*. The experiments were performed by John T. Mihalczko and coworkers. Some criticality safety measurements at these facilities have already been documented in the NEA *International Handbook of Evaluated Criticality Safety Benchmark Experiments* (list given in Appendix A). In many cases these experiments included reactor physics measurements. Some of these reactor physics measurements have also been documented in the literature, and this report give a complete list of references (Appendix B) for which John T. Mihalczko was an author or co-author. The experiments are divided into four classes: critical experiments only, critical and subsequent subcritical experiments, subcritical experiments at critical facilities, and subcritical measurements performed in material balance areas of the Y-12 NSC and other facilities. Because of the high cost and large amount of facility time related to these measurements, it is very cost-effective to mine the existing data to produce NEA reactor physics benchmarks. The information for many of these measurements is documented in critical experiment and subcritical experiment logbooks at the International Criticality Safety Benchmark Program at Idaho National Laboratory and in laboratory records at Oak Ridge National Laboratory.

2. REACTOR PHYSICS MEASUREMENTS

This section lists the various reactor physics that have been performed by John T. Mihalczko and co-workers, some of which have been described in the references. The majority of these measurements were performed at the ORCEF, but measurements at a total of eight DOE facilities are also included.

2.1 MIXTURES OF LOW ENRICHED UF₄ AND PARRAFIN

These experiments were performed at the ORCEF starting in 1959 and the early 1960s, and they included reactor physics measurements of the fast fission factor, which is related to the number of fissions occurring at high energy; foil activation, which measured the spatial distribution of the neutron flux; cadmium ratios, which are the ratios of the activation of a bare foil minus the activation of a cadmium-covered foil divided by the activation of a bare foil; extrapolation distance, buckling, and reflector savings; the infinite medium neutron multiplication factor determined at ORCEF and the Physical Constants Testing Reactor at Pacific Northwest National Laboratory (PNNL); the neutron age and nonleakage probability; and the prompt neutron time decay using a 150 keV Cockcroft Walton accelerator. Some of these data could be evaluated NEA reactor physics benchmarks. Some of these quantities—such as the fast fission factor, cadmium ratios, and the prompt neutron decay—are neutron spectrum dependent quantities and characterize the neutron spectrum. Some of criticality safety aspects of this work have been benchmarked in the NEA *International Handbook of Evaluated Criticality Safety Benchmark Experiments* (document number LEU-COMP-THERM-033). Much of the information in the criticality safety benchmark can be used to describe the system in the reactor physics benchmark.

2.2 REACTOR PHYSICS MEASUREMENTS FOR THE DESIGN OF THE HEALTH PHYSICS RESEARCH REACTOR

In 1960, delayed critical experiments with 93.2 wt. % ²³⁵U enriched uranium molybdenum (10 wt. % Mo) alloy were performed to benchmark calculational methods for the design of the Health Physics Research Reactor. In these measurements many reactor physics measurements were performed relative to the design of the reactor. The fissile materials were annular 8 in. outside diameter, 5-25/32 in. inside diameter metal plates of thicknesses varying from 1/8 to 1 in. with some special pie-shaped pieces that were 1/32 in. thick. There were cylindrical alloy plugs (5 23/32 in. outside diameter) for filling the central holes in the annular plates. The following reactor physics measurements were performed: prompt neutron time decay using the pulsed neutron method, radial and axial distribution of the fission density, reactivity associated with height change, central reactivity worth, reflection effects, effect of cadmium between the core and reflector, and effects of Plexiglas in the annulus center.

2.3 SPACE POWER REACTOR EXPERIMENTS

In the early 1960s, an unmoderated graphite reflected critical assembly of UO₂ (93.2 wt. % ²³⁵U enriched) fuel pins was assembled as part of the development of a space power reactor. A system with a beryllium reflector was also assembled. The UO₂ pellet density was 9.71 g/cm³, and the pellets were contained in two hundred and fifty-three 1.27 cm diameter and 30.48 cm long stainless-steel tubes with a center-to-center spacing of 1.506 cm in an aluminum container with a 25.96 cm diameter. This reactor core mock-up was also assembled with a beryllium reflector. The criticality safety data from these measurements were benchmarked in the NEA *International Handbook of Evaluated Criticality Safety Benchmark Experiments* with documents numbers SCCA-SPACE-EXP-001 and SCCA-FUND-EXP-001.

The following reactor physics measurements were used with these reactor mock-ups: axial and radial flux distributions from foil activation measurements in the core and reflector, axial and radial distributions of the cadmium ratios (bare foil activation minus activation of a cadmium covered foil divided by the activity of the bare foil), reactivity worth of the central fuel pin and fuel pins as a function of radial position in the core and reflector, reactivity worth of the graphite reflector plugs. Reactivity coefficients of rods (0.317 cm diameter) in the core of stainless steel (90 of 1,704 g and 46 of 871 g), tungsten (40 of 2,110 g), graphite (23 of 82 g), polyethylene (8 of 18.4 g), and niobium (46 of 1,050 g) were measured. The reactivity associated with outward displacement of the outer 20 fuel pins, potassium reactivity

coefficient in the core, and the reactivity worth of a B₄C (30.5 g) in the central fuel pin location. These measurements could be reactor physics benchmarks.

2.4 SORA REACTOR EXPERIMENTS

A mock-up of the proposed Sorgente Rapida (SORA) reactor, which was a repetitively pulsed reactor that served as a source of thermal neutrons for neutron scattering experiments at ORCEF. The system was brought to above delayed criticality by a rotating beryllium reflector. Neutrons from the fast core were moderated in polyethylene in the iron reflector. The following reactor physics measurements performed with this system could be used as NEA benchmarks: the reactivity of the beryllium reflector as a function of position relative to the reactor core, the fission rate distribution throughout the core used to obtain the peak-to-average power density, the thermal neutron fluence at the outer surface if the polyethylene scatterer in the reflector per fission in the core, and the prompt neutron decay constant as a function of reactivity. In addition, dynamic experiments were performed as a function of reactivity above delayed criticality. The static SORA reactor experiments have been documented in the NEA *International Handbook of Evaluated Criticality Safety Benchmark Experiments* in HEU-MET-FAST-096.

2.5 OAK RIDGE URANIUM METAL SPHERE

This uranium (~93.2 wt. % ²³⁵U) metal sphere was more spherical than Godiva and the critical configuration has been documented Nuclear Energy Benchmark HEU-MET-FAST-100. The following reactor physics measurements were performed with this system and could be used as NEA benchmarks: central uranium metal reactivity worth, fission rate spatial distributions, fission neutron importance spatial distributions, prompt neutron decay constant by the Rossi- α technique, and effective delayed neutron fraction.

2.6 INTERACTING URANIUM METAL CYLINDERS

Interacting enriched uranium metal coaxial cylinders with their flat surfaces parallel were assembled to delayed criticality. The diameters of the cylinders were 7, 11, and 15 in. with the thickness varied. The spacing between cylinders were as large as 52 in., and the reactivity of the individual cylinders was as high as 65 cents subcritical. The following reactor physics measurements performed with this system could be used as NEA benchmarks: the reactivity worth associated with a change in spacing between cylinders, the prompt neutron decay constant by the Rossi- α technique and axial fission rate distributions in the uranium metal and in the space between cylinders. For systems with large spacing, the axial distributions were very sensitive to small differences in reactivity of each cylinder. Small change in reactivity of the individual cylinders produced large changes in the axial fission rate distributions. The prompt neutron decay constants depended on the spacing between cylinders because the flight time between cylinders is a large part of the prompt neutron lifetime. A nuclear criticality safety benchmark for the interacting 11 in. diameter cylinders is given in HEU-MET-FAST-051.

2.7 ORNL MEASUREMENTS IN FLATOP AND JEZEBEL

In 1971, Oak Ridge National Laboratory (ORNL) performed measurements at LANL with JEZEBEL and with FLATTOP using an enriched uranium metal core and a plutonium metal core. The following reactor physics measurements performed with these systems could be used as NEA benchmarks: Cf source-driven noise analysis measurements near delayed criticality to determine the effective delayed neutron fraction, spatial distribution of the fission density, spatial distribution of the neutron importance, and Rossi- α measurements of the prompt neutron time behavior.

2.8 LANL JEMIMA PLATES WITH POLYETHYLENE AT ORCEF

These critical and subcritical measurements used the JEMIMA at LANL and 0.12 in. thick HEU metal cylinders with varying thicknesses of polyethylene (1/16, 1/8, 1/4, 3/8, 1/2, 1, 1 1/2, 2, and 2 3/8 in.) between the plates. The measurements were performed on the ORCEF vertical assembly machine. Partial pie-shaped pieces were available for adjustment to delayed criticality. Rossi- α and randomly pulsed neutron measurements with a time-tagged Cf source were performed at delayed criticality and at a variety of subcritical configurations. The LANL JEMIMA uranium metal plates were assembled to delayed critical and subcritical configurations with polyethylene measuring from 1/16 to 1 in. thick between them.

The following reactor physics measurements performed with these systems could be used as NEA benchmarks: Cf source-driven noise analysis measurements at critical and subcritical and Rossi- α measurements of the prompt neutron time behavior. Break-frequency noise analysis interpretation was performed to determine the subcriticality that was compared to Cf source-driven noise analysis measurements of the subcriticality. The nuclear criticality safety benchmark for the unmoderated and unreflected JEMIMA plates is given in HEU-MET-FAST-001.

2.9 WINCO STORAGE TANK EXPERIMENTS AT LANL

These experiments were with two flat coaxial cylindrical uranyl nitrate tanks separated in air in support of storage of uranium solutions at Idaho National Laboratory. The neutron multiplication factor varied from 1.000 at a spacing of 9.6 cm to 0.80 at a spacing of 57.9 cm. The following reactor physics measurements performed with these systems could be used as NEA benchmarks are: Cf source-driven noise analysis measurements at critical and subcritical and Rossi- α measurements of the prompt neutron time behavior at delayed criticality and varying subcriticalities. Break-frequency noise analysis interpretation was performed to determine the subcriticality that was compared to Cf source-driven noise analysis measurements of the subcriticality and agreed very well. Some of these subcritical measurements were a nuclear criticality safety benchmark and are given in SUB-HEU-SOL-THERM-002.

2.10 URANYL NITRATE SOLUTION TANK WITH VARYING CONCENTRATION

The solution concentration of uranium (93.16 wt. % ^{235}U) in the uranyl nitrate solution was varied in 15 steps from 13.7 g $^{235}\text{U}/\text{L}$ to 0.3 g/L and then to 0.0 (water). To minimize the handling hazard, the solution had no free acid content. The inside diameter of the tank was 30.48 in. and was filled to a height of 14.5 in. The neutron multiplication factor, k_{eff} , varied from 0.9 to 0. Californium source-driven noise-analysis measurements (~ 160) were collected at each solution concentration with a variety of detectors, detector locations, and source locations. In the solution, two ^3He proportional counters in aluminum tubes were used and external to the tank, plastic, and liquid scintillators.

The following reactor physics measurements performed with these systems could be used as NEA benchmarks: Cf source-driven subcritical noise analysis measurements and Rossi- α measurements of the prompt neutron time behavior.

2.11 TWO INTERACTING URANYL NITRATE SOLUTION TANKS

Californium source-driven noise analysis measurements were performed for subcritical configurations of two cylindrical tanks with their axes parallel. The tanks were filled with 480 g/L aqueous solution of highly enriched uranyl nitrate to a height of 90 cm. The separation between the tanks was varied from contact to 40 in. After initial measurement, the solution in one tank was diluted to 140 g/L and measurements were performed. Then the concentration of the solution in both tanks was 140 g/L, and measurements were performed. At one stage, measurements were performed with one tank full to 90 cm

and the other tank half full. Measurements were also performed as the tanks were initially filled as a function of height.

The following reactor physics measurements performed with these systems could be used as NEA benchmarks: Cf source-driven subcritical noise analysis measurements and Rossi- α measurements of the prompt neutron time behavior.

2.12 URANYL NITRATE SAFE STORAGE BOTTLES

These subcritical measurements with up to six 5 in. diameter “safe” storage bottles of aqueous uranyl nitrate solution located in close contact and separated used the Cf source-driven noise analysis method. Measurements were performed at a variety of source locations and with ^3He proportional counters at a variety of locations and adjacent to the bottles. The solution concentration was in grams per liter with no free acid content; the enrichment was the density in grams per cubic centimeter. The configurations included a linear array of one to three bottles, a triangular array of three bottles, and square arrays of four and six bottles. The spacing between the bottles was varied. Neutron multiplication factors for six bottles in a square array were as high as 0.95, and for a single bottle they were as low as 0.3.

The following reactor physics measurements performed with these systems could be used as NEA benchmarks: Cf source-driven subcritical noise analysis measurements and Rossi- α measurements of the prompt neutron time behavior.

2.13 MIXED URANIUM-PLUTONIUM CYLINDRICAL SOLUTION TANK AT PNNL

These measurements were performed with a stainless-steel cylindrical tank (13.93-in. inside diameter with a wall thickness of 0.031 in.) of mixed uranyl (127 g/L) and plutonium (255 g/L) nitrate 5.4 M solution. The initial measurements were at delayed criticality, and the solution height was reduced in steps down to 4.0 in. The Cf source-driven noise analysis measurements were performed with the source located on the external surface of the tank, and after the initial measurements, a thin-walled tube was inserted on the axis of the tank so that the source could be centrally located in the tank. With an external source, the measurements were performed at the critical height of 20.9 in., and 10 measurements were performed down to a solution height of 7.06 in. For the central source location, measurements were performed at the critical height of 23.89 in., and 10 were performed down to a solution height of 4 in.

The following reactor physics measurements performed with these systems could be used as NEA benchmarks: Cf source-driven noise analysis measurements at critical and subcritical, Rossi- α measurements of the prompt neutron time behavior. Break-frequency noise analysis interpretation was performed to determine the subcriticality that was compared to Cf source-driven noise analysis measurements of the subcriticality.

2.14 MIXED URANIUM-PLUTONIUM ANNULAR SOLUTION TANK AT PNNL

A series of experiments were performed in annular tank geometry using a mixed aqueous plutonium-uranium nitrate with 173 and 262 g/L of plutonium and depleted uranium, respectively. The height of the solution in the 53.34 cm outside diameter, 25.4 cm inside diameter, 106.68 cm high tank was varied from 73.8 cm at delayed criticality down to 23 cm, and the k_{eff} value varied from delayed criticality down to 0.70. The plutonium contained 91.1 wt. % ^{239}Pu , and the depleted uranium contained 0.57 wt. % ^{235}U . Californium source-driven noise analysis measurements were performed at delayed criticality and as the height was reduced. Subcritical measurements were also performed by the inverse kinetics methods slightly below delayed criticality, and break-frequency noise analysis measurements were performed for k_{eff} values as low as 0.70. The results were compared.

The following reactor physics measurements performed with these systems could be used as NEA benchmarks: Cf source-driven noise analysis measurements at critical and subcritical, Rossi- α measurements of the prompt neutron time behavior. Break-frequency noise analysis interpretation was performed to determine the subcriticality that was compared to Cf source-driven noise analysis measurements of the subcriticality.

2.15 MIXED URANIUM-PLUTONIUM SLAB SOLUTION TANK AT PNNL

A series of experiments were performed in slab geometry using a mixed aqueous plutonium-uranium nitrate with 173 and 262 g/L of plutonium and depleted uranium, respectively. Both the thickness of the slab for a fixed height of ~71 cm and the height for a fixed thickness of 19.05 cm were varied. The base length of the slab was 106.7 cm. The plutonium contained 91.1 wt. % ^{239}Pu , and the depleted uranium contained 0.57 wt. % ^{235}U . Cf source-driven noise analysis measurements were performed at delayed criticality as the height was reduced in both configurations to a variety of subcritical configurations with k_{eff} values as low as 0.70. Subcritical measurements were also performed by the inverse kinetics methods slightly below delayed criticality and break-frequency noise analysis for k_{eff} values as low as 0.70, and the results were compared.

The following reactor physics measurements performed with these systems could be used as NEA benchmarks: Cf source-driven noise analysis measurements at critical and subcritical, Rossi- α measurements of the prompt neutron time behavior. Break-frequency noise analysis interpretation was performed to determine the subcriticality that was compared to Cf source-driven noise analysis measurements of the subcriticality.

2.16 SUBCRITICAL MEASUREMENT WITH TWO INTERACTING URANYL NITRATE SOLUTION TANKS

Californium source-driven noise analysis measurements were performed for subcritical configurations of two cylindrical tanks with their axes parallel. The tanks were filled with 480 g/L aqueous solution of highly enriched uranyl nitrate to a height of 90 cm. The separation between the tanks was varied from contact to 40 in. After initial measurement, the solution in one tank was diluted to 140 g/L and measurements performed. Then the concentration of the solution in both tanks was 140 g/L, and measurements were performed. At one stage, measurements were performed with one tank full to 90 cm and the other tank half full. Measurements were also performed as the tanks were initially filled as a function of height.

The following reactor physics measurements performed with these systems that could be NEA benchmarks are: Cf source-driven subcritical noise analysis measurements, Rossi- α measurements of the prompt neutron time behavior.

2.17 SUBCRITICAL MEASUREMENT WITH HEU URANYL NITRATE SAFE STORAGE BOTTLES

These subcritical measurements with up to six 5 in. diameter “safe” storage bottles of aqueous uranyl nitrate solution located in close contact and separated used the Cf source-driven noise analysis method. Measurement were performed at a variety of source locations and with ^3He proportional counters at a variety of locations and adjacent to the bottles. The solution concentration was in grams per liter with no free acid content; the enrichment was the density in grams per cubic centiliter. The configurations were a linear array of one to three bottles, a triangular array of three bottles, square arrays of four and six bottles. The spacing between the bottles was varied. neutron multiplication factors for six bottles in a square array were as high as 0.95 and for a single bottle as low as 0.3.

The following reactor physics measurements performed with these systems could be used as NEA benchmarks: Cf source-driven subcritical noise analysis measurements and Rossi- α measurements of the prompt neutron time behavior.

2.18 SUBCRITICAL MEASUREMENT WITH HIGHLY ENRICHED URANIUM HYDRIDE CYLINDERS

Californium source-driven noise analysis subcritical measurements were performed on July 6–7, 1989, by ORNL at the LANL Critical Experiments Facility for unreflected ~15.0 cm diameter uranium (~91 wt. % ^{235}U enriched) hydride (H/U ratio of 3) with cylinders of varying heights. The UH_3 powder was in thin cylindrical stainless-steel cans with a density of the hydride of ~10 g/cm³. The enrichment of the uranium metal to make the hydride was 93.15 wt. % ^{235}U . Four 3.00 cm high (identified as I, II, III, and IV) and two 2.0 cm high (identified as A and B) hydride canned cylinders were available. The 0.5 cm thick steel table on which the configurations were assembled was located 3 m from the nearest two walls. The hydride cylinders were stacked on a 0.5 cm thick table 86 cm above the concrete floor. Configurations of cylinders 11, 14, and 16 cm high were assembled with nominal heights of 12, 14, and 16 cm and masses of 22,676, 26,264, and 29,858 g (including the steel cans), respectively.

The following reactor physics measurements performed with these systems could be used as NEA benchmarks: Cf source-driven subcritical noise analysis measurements of the subcriticality and Rossi- α measurements of the prompt neutron time behavior.

2.19 SUBCRITICAL MEASUREMENTS WITH HEU CASTINGS IN A CONCRETE STORAGE VAULT

Californium source-driven frequency analysis measurements for a highly enriched uranium (HEU) (~93.2) metal storage vault at the Oak Ridge Y-12 NSC were performed to provide data for verification of calculational methods for criticality safety and to assess the effects of any loss of unbound water from the concrete. The measurements showed that $3 \times 3 \times 10$ arrays of ~18 kg uranium annular castings are essentially infinite because the results for the $5 \times 5 \times 10$ arrays are not statistically different from those of the smaller arrays. These measured frequency analysis parameters are presented and inferred subcritical neutron multiplication factors from the measurement are compared with the calculations.

The following reactor physics measurements performed with these systems could be used as NEA benchmarks: Cf source-driven subcritical noise analysis measurements, Rossi- α and randomly pulsed neutron measurements of the prompt neutron time behavior, spatial distribution of the neutron importance, and spatial distribution of the fission density.

2.20 SUBCRITICAL MEASUREMENTS WITH TWO HIGHLY ENRICHED URANIUM METAL CYLINDERS WITH VARYING MATERIALS BETWEEN THEM

Materials of varying thicknesses that were of interest to nuclear criticality safety were placed between two coaxial canned HEU metal cylinders of 6 in. diameter, and a variety of measurements were taken using the Cf source-driven noise analysis method.

The following reactor physics measurements performed with these systems could be used as NEA benchmarks: Cf source-driven subcritical noise analysis measurements, and Rossi- α and randomly pulsed neutron measurements of the prompt neutron time behavior

2.21 SUBCRITICAL INTERACTING HEU URANIUM METAL SEPARATED BY VARYING THICKNESSES OF BOROPLASTER

Californium source-driven noise analysis subcriticality measurements were performed for interaction experiments with varying thicknesses (0.38–5.7 in.) of boroplaster (each boroplaster was ~0.38 in. thick with a diameter of 7 in.) between 7-in.-diameter HEU metal cylinders.

The following reactor physics measurements performed with these systems could be used as NEA benchmarks: Cf source-driven subcritical noise analysis measurements and Rossi- α and randomly pulsed neutron measurements of the prompt neutron time behavior.

2.22 SUBCRITICAL MEASUREMENT WITH UP TO FIVE ADJACENT UNREFLECTED HEU CASTINGS

These measurements for Y-12 NSC nuclear criticality safety involved up to 90 kg of uranium (93.2 wt. % ^{235}U) metal castings. Each of the annular castings had an outside diameter of 5 in., an inside diameter of 3.5 in., a height of 6 in., and weighed about 18 kg. Each was contained in stainless-steel cans for contamination control. Active interrogation measurement with 1, 2, 3, 4, and 5 adjacent castings (>2) were performed both with a time tagged Cf source and a DT neutron generator. The measurements were performed with four $1 \times 1 \times 6$ in. long plastic scintillators adjacent to the casting in a variety of locations, with the long dimensions parallel to the axis of the casting.

The following reactor physics measurements performed with these systems could be used as NEA benchmarks: Cf source-driven subcritical noise analysis measurements and Rossi- α , randomly pulsed neutron and accelerator-driven measurements of the prompt neutron time behavior.

3. CONCLUSIONS

This report details a wide variety of data that can be mined for Nuclear Energy Agency reactor physics benchmarks. The acquisition of these data required a large amount of critical facility operational time that has been documented and, in many cases, could not be repeated due to costs, approval processes, and availability of fissile material. The experiments were performed by John T. Mihalcz and coworkers at many eight DOE facilities including ORCEF (between 1958 and 1975); Los Alamos National Laboratory; Pacific Northwest National Laboratory; Babcock and Wilcox at Lynchburg, Virginia; and the Y-12 National Security Complex (the latter between 1975 and up to 2006). Some criticality safety measurements at these facilities have already been documented in the NEA *International Handbook of evaluated Criticality Safety Benchmark Experiments*. Some of these reactor physics measurements have also been documented in the literature, and this document give a complete list of references for which John T. Mihalcz was an author or co-author. The experiments are divided into four classes: critical experiments only, critical and subsequent subcritical experiments, subcritical experiments at critical facilities, and subcritical measurements performed in material balance areas of Y-12 NSC and other facilities. Because of the high cost and large amount of facility time related to these measurements, it is very cost-effective to mine the existing data to produce NEA reactor physics benchmarks. The information for many of the measurements is documented in critical experiment and subcritical experiment logbooks at the International Criticality Safety Benchmark Program at Idaho National Laboratory and in laboratory records at ORNL.

APPENDIX A. HANDBOOK OF EVALUATED CRITICALITY SAFETY BENCHMARK EXPERIMENTS

The following experiments have been included by the Nuclear Energy Agency's *International Handbook of Evaluated Criticality Safety Benchmark Experiments*.

Identifier	Experimenter	Title
HEU-MET-FAST-003	Mihalcz	Complex Geometry Bare Orallo (93.15 ²³⁵ U) Metal Annuli Experiments
HEU-MET-FAST-007	Mihalcz	Uranium Metal Slabs Moderated with Polyethylene, Plexiglas and Teflon
HEU-MET-FAST-051	Mihalcz	Uranium (93.2) Metal Cylinders (7-Inch, 9- Inch, 11-Inch, 13-Inch, 15-Inch Diameter Cylinders and Two 11-Inch Diameter Interacting Uranium (93.2) Metal Cylinders
HEU-MET-FAST-059	Mihalcz	Orallo (93.15 ²³⁵ U) Metal Annuli with Beryllium Core
HEU-MET-FAST-061	Mihalcz	Orallo (93.2 ²³⁵ U) Metal Cylinder with Beryllium Top Reflector
HEU-MET-FAST-071	Mihalcz	Uranium (93.14) Metal Annuli with One- And Two-Inch Graphite Reflectors
HEU-MET-FAST-074	Mihalcz	Orallo (93.2 ²³⁵ U) Bare Metal Annuli and Disks
HEU-MET-FAST-076	Mihalcz	Uranium (93.14 ²³⁵ U) Metal Annuli and Cylinders with Thick Polyethylene Reflectors and/or Internal Polyethylene Moderator
HEU-MET-FAST-077	Mihalcz	Experiments with HEU (93.14 wt. %) Metal Annuli with Internal Graphite Cylinders
HEU-MET-FAST-081	Mihalcz	Grotesque: Complex Geometric Arrangement of Unreflected HEU (93.15) Metal
HEU-MET-FAST-083	Mihalcz	Complex Geometry Bare Orallo (93.15 ²³⁵ U) Metal Annuli Experiments
HEU-MET-FAST-096	Mihalcz	Static Critical Experiments for The Sorgente Rapida (Sora) Reactor Mockup
HEU-MET-FAST-099	Mihalcz	Fast Neutron Spectrum Potassium Worth for Space Power Reactor Design Validation (also known as ORCEF-SPACE-EXP-001)
HEU-MET-FAST-100	Mihalcz	Orsphere: Critical, Bare, HEU (93.2)-Metal Sphere
SCCA-SPACE-EXP-001	Mihalcz	Critical Configuration and Physics Measurements for Assemblies of U(93.15)O ₂ Fuel Rods
HEU-COMP-FAST-002	Mihalcz	Critical Configuration and Physic Measurements for Graphite Reflected Assemblies of U(93.15)O ₂ Fuel Rods (1.506-cm Pitch)
HEU-COMP-FAST-004	Mihalcz	Critical Configuration for Beryllium Reflected Assemblies of U(93.15)O ₂ Fuel Rods (1.506-CM Pitch and 7-Tube Clusters)
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SUB-HEU-SOL-THERM-002	Mihalcz	Subcritical Noise Measurements for a Two Coaxial Cylindrical Tanks Containing 93.1 Uranyl Nitrate Solution

APPENDIX B. REFERENCES

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